

# SET A

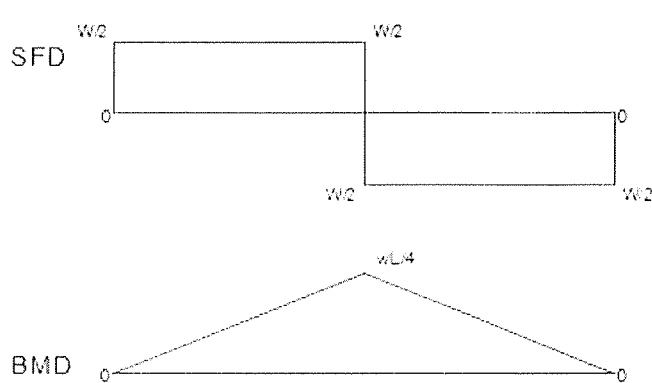
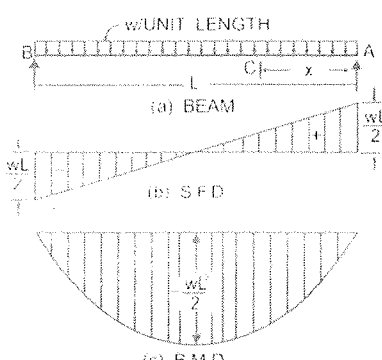
## Scoring Indicator

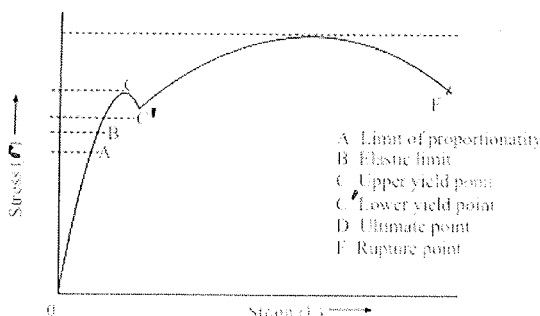
Course Name: **Strength of materials**

Course Code: *Rev(21)-3021*

QID: *2110 220174*

Q.No	Scoring Indicator	Split Score	Sub Total	Total Score
	PART - A			9
I.1	Hardness		1	
I.2	$E=2G(1+\mu)$		1	
I.3	$^{\circ}\text{C}$		1	
I.4	Shear force <del>diagram</del>		1	
I.5	<del>Force</del> $F = dM/dx$		1	
I.6	$l/d$		1	
I.7	long		1	
I.8	$D/d$		1	
I.9	two		1	
	PART - B			24
II.1	Malleability: Malleability is the property of metal associated with the ability to be hammered into a thin sheet.	1.5	3	
	Ductility: Ability of material to deform under tensile load.	1.5		
II.2	Factor Safety = Ultimate stress/Working stress	1.5	3	
	Explanation	1.5		
II.3	Statement: Within the elastic limit, stress is directly proportional to strain	1.5	3	
	Equation: (Stress/Strain = E)	1.5		
II.4	Young's Modulus: Tensile or compressive stress/Strain	1	3	
	Modulus of rigidity = Shear stress/Shear Strain	1		
	Bulk Modulus = Direct stress/Volumetric strain	1		

II.5	 <p>SFD</p> <p>BMD</p>	1.5		
II.6	 <p>(a) BEAM</p> <p>(b) SFD</p> <p>(c) BMD.</p>	1.5	3	
II.7	<p>Definition: The minimum axial load at which the column tends to have lateral displacement is called buckling load.</p> <p>Euler's formula: <math>\pi^2 EI / l^2</math></p>	1.5	3	
II.8	<p>Definition: Polar moment of inertia of a plane area is basically defined as the area moment of inertia about an axis perpendicular to the plane of figure and passing through the center of gravity of the area.</p> <p>Formula: <math>\pi(D^4 - d^4)/32</math></p>	1.5	3	
II.9	<p>Solid length = <math>nd</math></p> <p>Free length = solid length + max. compression + clearance</p> <p>Spring stiffness = <math>W/\delta</math></p>	1 1 1	3	

II.10	Hoop stress, $\sigma_h = pd/2t$ $\rightarrow t = pd/2\sigma_h$ $= 2 \times 1000 / 2 \times 100$ $= 10 \text{ mm}$	1.5  1.5	3	
PART - C				42
III.1		Fig. (3)  Mark ings (4)	7	
III.2	1. Stress, $\sigma = P/A = 30 \times 1000 / (\pi/4) \times 30^2 = 42.44 \text{ N/mm}^2$ . 2. $\sigma/e = E \rightarrow e = \sigma/E = 42.44 / 2 \times 10^5 = 0.000212$ 3. $\delta l = PL/AE = 30 \times 1000 \times 2000 / (\pi/4) \times 30^2 \times 2 \times 10^5 = 0.0424 \text{ mm}$	2 2 3	7	

III.3		1  3  3	7	
III.4	Point Load, Uniformly distributed load, Uniformly varying load  Figure Explanation	4 3	7	
III.5	Deflection at free end = $wl^4/8EI = Wl^3/8EI$ $= 15 \times 6 \times 1000 \times 6000^3 / 8 \times 2 \times 10^5 \times 95 \times 10^7$ $= 12.78 \text{ mm}$	Formula(3) Finding I(2) Ans (2)	7	
III.6	Both end hinged, One end hinged and other free, one end hinged and other fixed, both ends fixed  Figure Explanation	4 3	7	

III.7	$M = WL/4 = 100 \times 5/4 = 125 \text{ Nm.}$ $I = \pi(D^4 - d^4)/64 = 510508.8062$ $M/I = \sigma/y \rightarrow \sigma = My/I = 125 \times 1000 \times 30/510508.8062$ $= 7.34 \text{ N/mm}^2$	2 2 3	7	
III.8	<p>It is the ratio of moment of inertia of a section about the neutral axis to distance of the outermost layer from the neutral axis.</p> $Z = I/y_{\max}$ Section modulus for circular section: <del><math>\pi d^3/32</math></del> $\frac{\pi d^3}{32}$ Section modulus for hollow section: $\pi(D^4 - d^4)/32D$	2 2.5 2.5		
III.9	$T_{\text{solid}} = \pi \tau d^3/16$ $T_{\text{hollow}} = (\pi \tau/16) \times (65D^3/81)$ ; D = outside diameter of hollow shaft. $T_{\text{solid}} = T_{\text{hollow}} \rightarrow d = 0.929D$ $W_{\text{solid}} = \text{volume} \times \text{density} \times g = (\rho \times \pi d^2 l/4)g$ $W_{\text{hollow}} = \text{volume} \times \text{density} \times g = ((\rho \times 5\pi D^2 l)/36)g$ $W_{\text{solid}}/W_{\text{hollow}} = 1.55$	1 1 2 2 1	7	
III.10	$\sigma_h = pd/2t = 1.5 \times 1000/2 \times 20 = 75 \text{ N/mm}^2$ $\sigma_l = pd/4t = 1.5 \times 1000/4 \times 20 = 37.5 \text{ N/mm}^2$	3.5 3.5	7	
III.11				

Consider a circular shaft of radius  $R$  and length  $l$  rigidly fixed at one end A, and torque  $T$  is applied at free end as in Fig. 8.2(a)

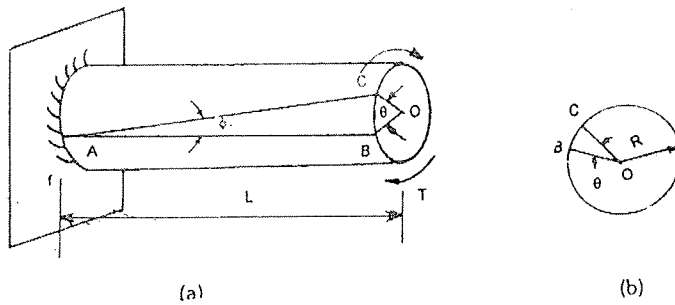


Fig. 8.2

As a result of torque line AB on the surface is changed to AC, and radius OB rotates to OC.

$$\text{Shear strain} = \frac{BC}{AB} = \tan \phi$$

Since  $\phi$  is very small,  $\tan \phi \approx \phi$

$$\therefore \text{Shear strain, } \phi = \frac{BC}{l} \quad \dots\dots\dots (i)$$

Also from Fig. 8.2(b)

$$BC = R \cdot \theta \quad \dots\dots\dots (ii)$$

Where  $\theta$  = Angle of twist, in radians

$R$  = Radius of the shaft

From equations (i) and (ii)

$$R \cdot \theta = \phi \cdot l$$

$$\text{or } \phi = \frac{R.\theta}{l}$$

But from definition,

$$\phi = \frac{\text{shear stress}}{\text{modulus of rigidity}}$$

$$\phi = \frac{\tau}{G}$$

$$\therefore \frac{\tau}{G} = \frac{R.\theta}{l}$$

$$\text{or } \tau = \frac{RG.\theta}{l}$$

For a given shaft and for a given torque, the values of  $G$ ,  $\theta$  and  $l$  are constant; therefore, the shear stress induced is proportional to radius

$$\text{i.e., } \frac{\tau}{R} = \text{constant}$$

Thus, if the 'q' is the shear stress induced at a radius,  $r$  from the centre,

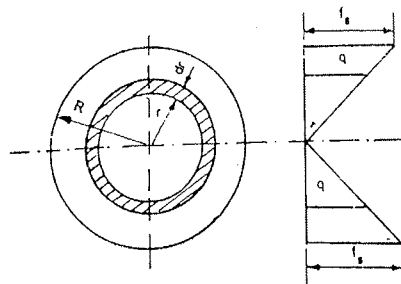
$$\frac{q}{r} = \frac{\tau}{R} = \text{constant}$$

$$\text{or } \frac{q}{r} = \frac{\tau}{R} = \frac{G\theta}{l} \quad \dots\dots\dots (1)$$

**Torque Transmitted by Shaft :** Consider a small ring of area  $dA$  at a distance ' $r$ '. The shear stress acting on the ring

$$q = \frac{\tau}{R} \cdot r$$

$$\text{Force on the ring, } dF = q \cdot dA = \frac{\tau}{R} \cdot r \, dA$$



$$\begin{aligned} \text{Torque due to } dF, \quad dT &= \frac{\tau}{R} q \cdot dA \cdot r \\ &= \frac{\tau}{R} \cdot r^2 dA \end{aligned}$$

$$\therefore \text{Total torque, } T = \frac{\tau}{R} \int r^2 dA$$

$$\rightarrow T = \frac{\tau}{R} J$$

$$\rightarrow \frac{T}{J} = \frac{\tau}{R} \quad \text{--- (2)}$$

$$\text{from (1) \& (2) } \quad \frac{T}{J} = \frac{\tau}{R} = \frac{G\theta}{l}$$

III.42	Helical spring (Explanation + fig.)	3.5	7	
	Laminated spring (Explanation + fig.)	3.5		